

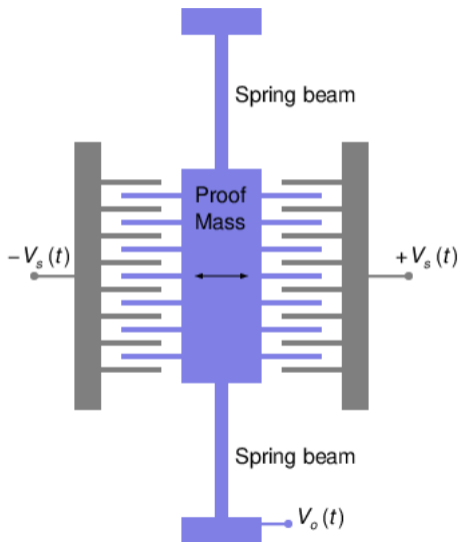
IN 221 (AUG) 3:0  
Sensors and Transducers  
Electromagnetic Sensors and Transducers  
Lecture 2

A. Mohanty

Department of Instrumentation and Applied Physics (IAP)  
Indian Institute of Science  
Bangalore 560012

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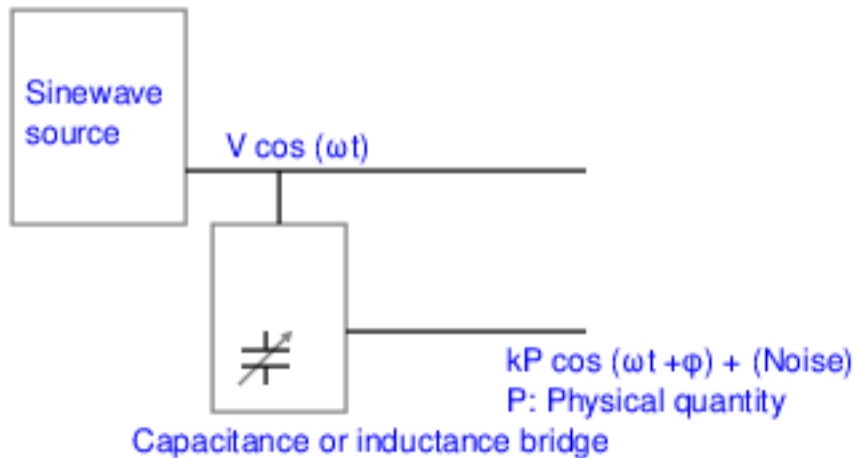
# Accelerometer: Interdigitated Structure



# Accelerometer or Pressure sensor

- A flexible electrode moves a small distance that is proportional to the acceleration or the pressure difference to be measured.
- This small movement changes a capacitance or an inductance.
- With a bridge arrangement, this sensor can be ...
  - ... sensitive,
  - ... reliable,
  - ... and quite linear.

# How do we measure $P$ ?



# How do we measure $P$ ?

Physical quantity to be measured:  $P$

Output: (Signal) + (Noise)

Signal:  $kP \cos(\omega t + \phi)$

$$v_o = kP \cos(\omega t + \phi) + (\text{Noise})$$

- The signal output may be quite small.
- It is still proportional to  $P$ .
- Here,  $\phi$  is a constant phase shift that is specific to the bridge instrumentation.

# Trouble with simple amplification

- In industrial settings, the noise strength may be comparable to the signal. It may sometimes be greater.
- If we simply amplify the output, the noise will also be amplified.
- Filtering will decrease the noise, but that may not be enough.
- Cases like this are very common.

# Lock-in Amplifier

- Solution: Use a *lock-in amplifier*.
- Other names:
  - Synchronous detection
  - Phase-sensitive detection
- Implementation: Multiply the bridge output  $v_o$  with the reference sinewave and average (low-pass filter) it.
- What is the resulting output?

# Lock-in Amplifier Mathematics

The output of the multiplier is

$$V \cos(\omega t) \times kP \cos(\omega t + \phi) = kVP[\cos(\phi) \cos^2(\omega t) - \sin(\phi) \sin(\omega t) \cos(\omega t)]. \quad (1)$$

$$\cos^2(\omega t) = \frac{1}{2} + \frac{\cos(2\omega t)}{2}, \quad (2)$$

and

$$\sin(\omega t) \cos(\omega t) = \frac{\sin(2\omega t)}{2}. \quad (3)$$

Both  $\cos(2\omega t)$  and  $\sin(2\omega t)$  have average value of 0.

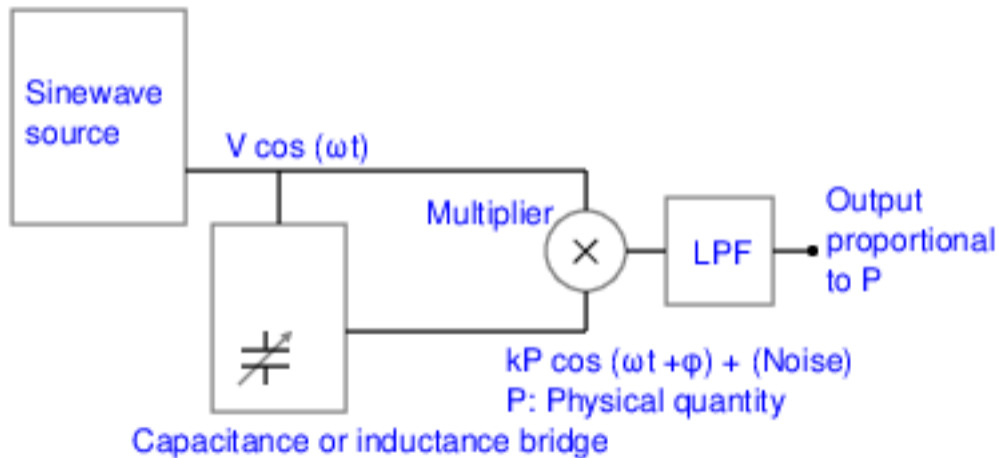
So the average value of  $\cos^2(\omega t)$  is  $\frac{1}{2}$ , and that of  $\sin(\omega t) \cos(\omega t)$  is 0.

The average value of the product is  $\frac{1}{2}kVP \cos(\phi)$ .  $\Rightarrow$  (LPF output)  $\propto P$ .

(If we are unlucky to have  $\cos \phi = 0$ , we can use  $V \sin(\omega t)$  instead of  $V \cos(\omega t)$  at one input of the multiplier.)



# Lock-in Amplifier: Block diagram

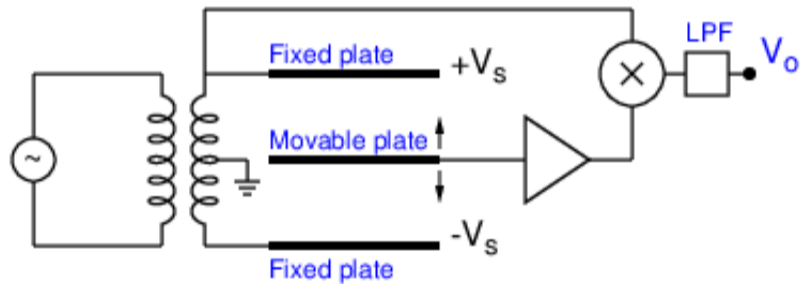


# Demonstration of a Lock-in Amplifier

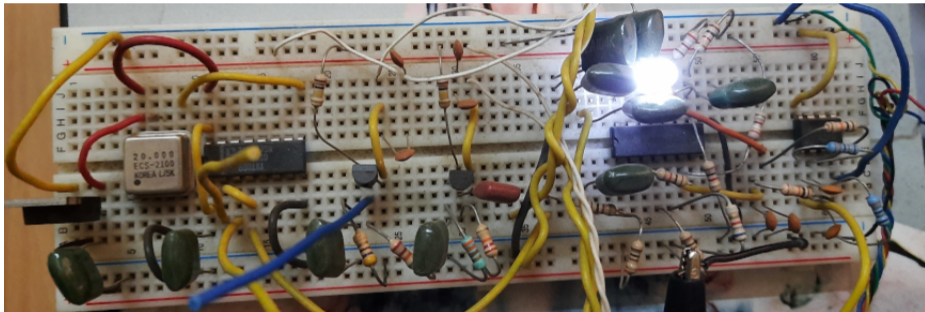
The following circuit shows how we may measure the difference between two small capacitances using a lock-in amplifier.

- Constructed on bread board.
- $\Delta C < 1 \text{ pF}$
- Layout not neat at all . . .
- . . .yet the output signal is very clean.

# Capacitive Sensor: Block Diagram



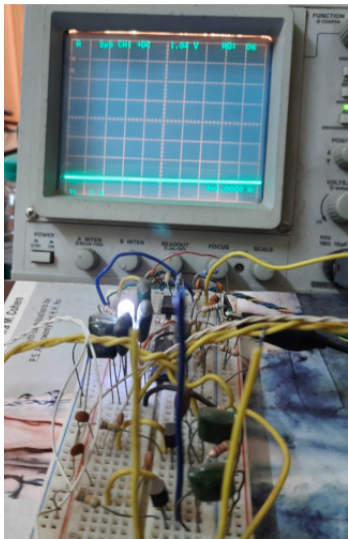
# Example Differential Capacitive Sensor



# Capacitive Sensor: Circuit Details

- 20 MHz crystal oscillator output given to a divide by 2 counter.
- 1/4 of 74LS175 D flip-flop used to implement the divide by 2 counter.
- $Q_0$  output is  $+V_s(t)$ ,  $\overline{Q_0}$  output is  $-V_s(t)$
- The two yellow wires sticking out are the fixed plates.
- The blue wire sticking out is the movable plate.
- The amplifier is a two-transistor tuned amplifier.
- MC1496 is used as the multiplier.
- Uses RC LPF.
- NE5532 is the final amplifier after the LPF.

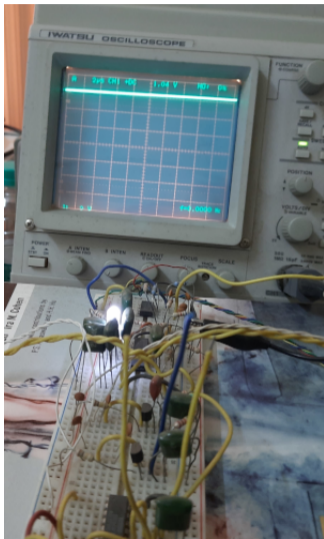
# Blue Wire Closer to the Left Yellow Wire



# Blue Wire Equidistant from the Yellow Wires



# Blue Wire Closer to the Right Yellow Wire





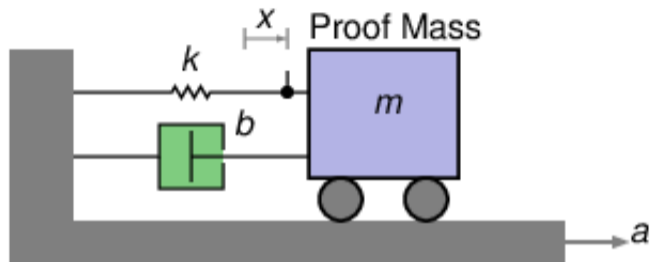
## What is an accelerometer?

- A sensor whose output is proportional to its acceleration, at least when the acceleration is changing slowly
- If the acceleration is changing too fast, then the output may not be able to keep up with the input.
- Accelerometers usually have three output channels for the three components of acceleration.
- Some accelerometers provide analogue voltage outputs, while others internally convert their outputs to a digital form.
- Accelerometers made using MEMS technology are very successful.

# Accelerometer: Applications

- Sensing the acceleration of aircraft and vehicles
- Sensing the orientation of hand-held devices using the acceleration due to gravity
- Sensing vibration in industrial applications

# Accelerometer: Modelling



Simplified Mass-Spring-Dashpot model

$x$ : Displacement of the mass from its equilibrium position in the frame of the accelerometer

$$m\ddot{x} = -kx - b\dot{x} - ma$$

$$m\ddot{x} + b\dot{x} + kx = -ma$$

(4)

# Accelerometer: Transfer Function

$$T(s) = \frac{X(s)}{A(s)} = \frac{-1}{s^2 + \frac{b}{m}s + \frac{k}{m}}$$

Note: The negative sign is due to my sign convention.

Many books will indicate  $x$  in the reverse direction to not have this negative sign.

$$T(s) = \frac{-1}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2}, \quad (5)$$

where,

$$\omega_0 = \sqrt{\frac{k}{m}}, \quad (6)$$

and

$$Q = \frac{\sqrt{km}}{b}. \quad (7)$$

# Accelerometer: Low Frequency Response

For  $\omega \ll \omega_0$ ,

$$T(j\omega) \approx \frac{-1}{\omega_0^2} = -\frac{m}{k}. \quad (8)$$

Typical value:  $f_0 = \frac{\omega_0}{2\pi} = 50 \text{ kHz}$

## Conclusions

- For frequencies which are small compared to the resonant frequency, the displacement is proportional to the acceleration.
- There is a need to make the electrical output proportional to  $x$ .

# Accelerometer: Sensing the Displacement

## Differential Capacitance Arrangement

- The proof mass acts as an electrode that moves between two other electrodes.
- It forms two capacitances that are equal when there is no displacement.
- The difference between the capacitances is proportional to the displacement, provided the displacement is small.

## Challenge

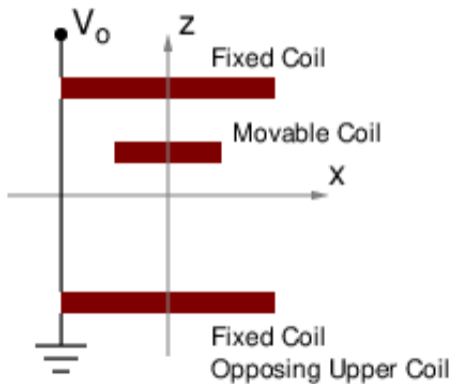
- The devices are very small.
- The change in capacitance is very small.
- How do we reliably detect this small change?
- Answer: Use lock-in amplifier.

Now we discuss the LVDT, a displacement sensor.

- Linear Variable Differential Transformer
- Two fixed coils in anti-series (in opposition)
- One movable coil
- Usually the movable coil is excited with sinewave AC.
- Fixed coil output is given to the phase sensitive detector.
- Quite robust and accurate

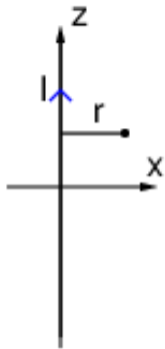
# LVDT Coils

## LVDT





# Magnetic Field due to Infinite Wire

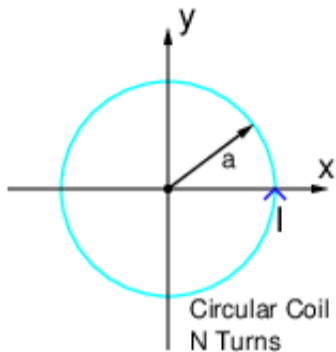


$$B_\phi = \frac{\mu_0 I}{2\pi r} \quad (9)$$

Magnetic constant:  $\mu_0 = 4\pi \times 10^{-7} \text{ T m / A}$

Example computation: If  $I = 10 \text{ A}$ , and  $r = 1 \text{ cm}$ , then  $B_\phi = 0.2 \text{ mT}$ .

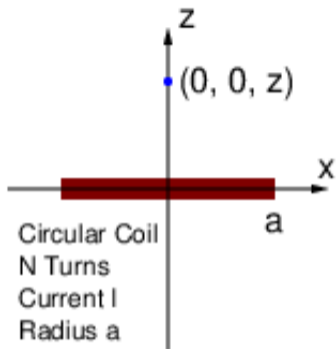
# Circular Coil: B at Centre



$$B_z(0, 0, 0) = N \frac{\mu_0 I}{2a} \quad (10)$$

Example computation: If  $N = 100$ ,  $I = 1$  A, and  $a = 5$  cm, then  
 $B_z(0, 0, 0) = 1.2566$  mT.

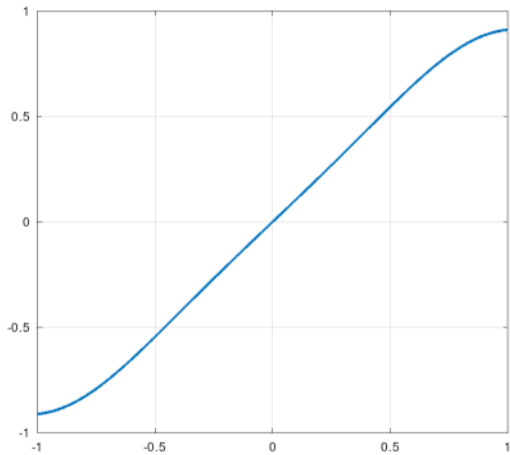
# Circular Coil: B on the Axis



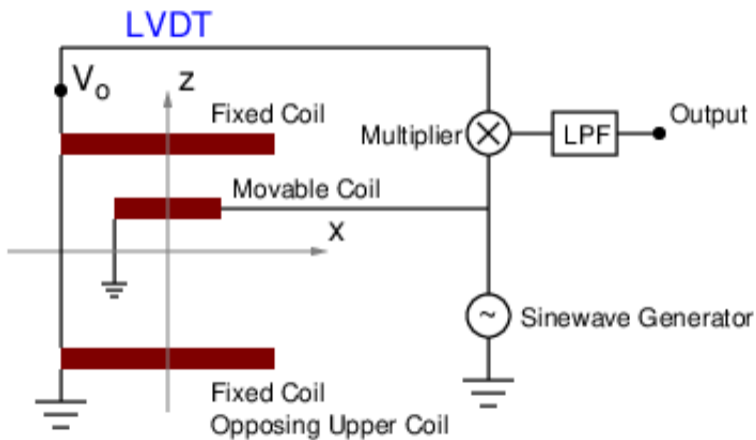
$$B_z(0, 0, z) = N \frac{\mu_0 I a^2}{2(a^2 + z^2)^{3/2}} \quad (11)$$

Example computation: If  $N = 100$ ,  $I = 1$  A,  $a = 5$  cm, and  $z = 5$  cm, then  
 $B_z(0, 0, z) = 0.444 29$  mT.

# LVDT Output Linearity



# LVDT Block Diagram



# LVDT Analysis

Detailed analysis of the LVDT requires the study of the following concepts.

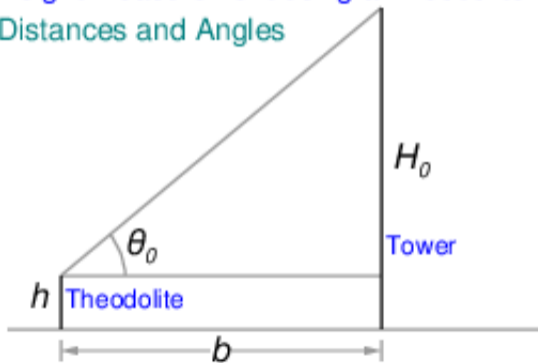
- Magnetic field of a coil
- Mutual inductance
- Lock-in amplifier

# Example of Error Analysis

We wish to measure the height of a tower using a theodolite.

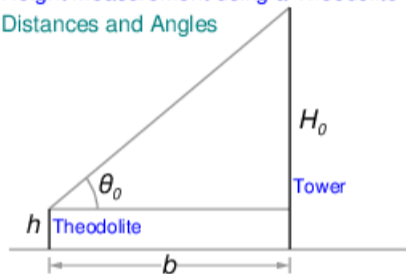
Height Measurement using a Theodolite

Distances and Angles



# Another Example of Error Analysis

Height Measurement using a Theodolite  
Distances and Angles



$$H_0 = h + b \tan \theta_0. \quad (12)$$

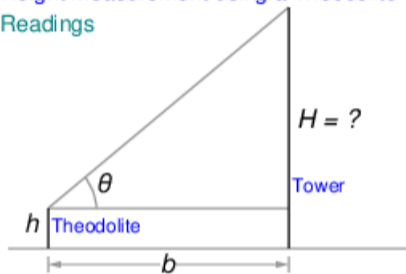
Note that

$$b = \frac{H_0 - h}{\tan \theta_0}. \quad (13)$$



# Measurements

Height Measurement using a Theodolite  
Readings



In actual measurement, the reading of the theodolite is  $\theta$ , which is not the same as  $\theta_0$  due to instrument errors. Also,  $h$  and  $b$  can be measured very accurately. So we consider the angle ( $\theta$ ) measurement as the only source of error.

Estimated height is

$$H = h + b \tan \theta. \quad (14)$$

# Error Analysis

Error in height is

$$H_0 - H = b(\tan \theta_0 - \tan \theta) \approx b \sec^2 \theta_0 \times (\theta_0 - \theta).$$

But

$$b = \frac{H_0 - h}{\tan \theta_0}.$$

So

$$H_0 - H \approx b \sec^2 \theta_0 \times (\theta_0 - \theta) = \frac{H_0 - h}{\tan \theta_0} \sec^2 \theta_0 \times (\theta_0 - \theta).$$

Or,

$$H_0 - H \approx \frac{H_0 - h}{\sin \theta_0 \cos \theta_0} \times (\theta_0 - \theta).$$

The error in angle measurement is magnified by a factor

$$K = \frac{H_0 - h}{\sin \theta_0 \cos \theta_0} = 2 \frac{H_0 - h}{\sin(2\theta_0)}. \quad (15)$$

What value of  $\theta_0$  minimizes  $K$ ?

# Answer

$\sin(2\theta_0)$  can be a maximum of 1, when  $\theta_0 = \pi/4$ .

So the answer is 45 degrees.

In other words,  $b$  should be as close to  $H_0 - h$  as possible.